# Influence of noise mechanism on zero-bias resistance junction-area product in In<sub>0.53</sub>Ga<sub>0.47</sub>As photovoltaic infrared detector

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We theoretically analyze the effects of material parameters on the  $R_0A$  product of  $In_{0.53}Ga_{0.47}As$  photovoltaic infrared detector by considering the four dominant noise mechanisms. The results show that  $R_0A$  is mainly affected by generation-recombination mechanism at the carrier concentration< $10^{15}$  cm<sup>-3</sup> for the triangular and parabolic potential barriers. Moreover, the effects of surface recombination velocity, its carrier concentration and thickness on  $R_0A$  product have also been discussed. The influence of *p*-region material parameters on the  $R_0A$  product is larger than that of the *n*-region.  $R_0A > 10^6 (\Omega \cdot cm^2)$  at  $p = 10^{17} cm^{-3}$ ,  $R_0A$  product of  $10^8 \Omega \cdot cm^2$  (T = 250K) and  $10^6 \Omega \cdot cm^2$  (T = 300K) are obtained.

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#### 1. Introduction

Modern high-performance infrared photovoltaic detector technology, based on photon absorption in narrow-gap semiconductors, has attracted much attention in near infrared applications, such as remote sensing and spectroscope analysis, infrared imaging, optical communication and many other fields. Indium Gallium Arsenide  $(In_{1-x}Ga_xAs)$  ternary alloys have become important materials for the fabrication of infrared detectors, due to their prominent features such as relatively low dark current density, quick response, as well as high sensitivity and detectivity. The energy gap of the  $In_{1-x}Ga_xAs$  ternary system spans from 0.35 eV (3.5 $\mu m$ ) for InAs to 1.43 eV $(0.87 \mu m)$  for GaAs.  $In_{0.53}Ga_{0.47}As$  alloy  $(E_g=0.73 \ eV)$ ,  $\lambda_c = 1.7 \mu m$ ) lattice matched to the *InP* substrate has already been proved to be a suitable detector material for near-infrared  $(1.0 \sim 1.7 \mu m)$  spectral range [1-4].

Dark current passing across detector will generate noise because of the statistical nature of the generation and recombination process. Mainly four-type noise mechanisms of infrared detector have been considered, including generation-recombination noise, radiative noise, Auger recombination noise and tunneling noise. Detectivity (denoted as  $D^*$ ) is an important parameter to measure detector performance, while the noise has great effect on  $D^*$ . Therefore, it is indispensable to suppress all kinds of noise mechanisms in order to improve the  $D^*$ . In this paper, we theoretically analyze the dependence of the zero-bias resistance junction-area product  $(R_0A)$  on material parameters [5-8].

# 2. Theoretical analysis

The calculation is based on a structure of photodetector, which can be simplified as a *p*-*n* type of  $In_{I-x}Ga_xAs$  deposited on InP substrate. The geometry of the photodetector is taken in Fig. 1. Usually, the performance of infrared photovoltaic detector is characterized by the detectivity  $D^*$ , which depends on the zero-bias resistance junction-area product ( $R_0A$ ) and quantum efficiency ( $\eta$ ) under negligible background radiation,

$$D^* = \frac{\lambda \eta q}{hc} \sqrt{\frac{R_0 A}{4kT}} \tag{1}$$

where  $\eta$  and k are quantum efficiency and Boltzmann constant, respectively.  $\lambda$  is the wavelength of the incidence light, *T* is the work temperature, *c* is the velocity of light and *q* is the charge of an electron.

All the noise mechanisms are independent. When four type noise mechanisms are considered,  $(R_0A)_{Total}$  can be expressed by [9]:

$$\frac{1}{(R_0 A)_{Total}} = \frac{1}{(R_0 A)_{Auger}} + \frac{1}{(R_0 A)_{GR}} + \frac{1}{(R_0 A)_{Rad}} + \frac{1}{(R_0 A)_{Tunnel}}$$
(2)

Where  $(R_0A)_{Auger}$ ,  $(R_0A)_{GR}$ ,  $(R_0A)_{Rad}$  and  $(R_0A)_{Tunnel}$  are determined by Auger recombination noise.

generation-recombination noise, radiative noise and tunneling noise.



Fig. 1. Schematic 2D structure of  $In_{1-x}Ga_xAs p$ -n junction. W is width of depletion region;  $W_n$  is width of depletion region on n side;  $W_p$  is width of depletion region on p side; t and d are n-region thickness and p-region thickness;  $S_h$  and  $S_e$  are surface recombination velocity for holes in n region and for electrons in p region; n and p are carrier concentration in n-region and p-region.

# 2.1 Auger recombination mechanism and Radiative mechanism

Auger recombination mechanism and radiative mechanism are mainly depended on the processes of generation-recombination during the diffusion of minority carriers. Therefore, for Auger recombination mechanism and radiative mechanism, the equations of diffusion current and  $R_0A$  are identical with each other. However, the lifetime of minority carriers in p-n junction is different.

There are 10 ways about the Auger recombination mechanism. Among them, CCCH, CHHL and CHHS are three fundamental ones. The lifetime of CCCH, CHHL and CHHS in *p*-region and *n*-region can be indicated by [10]:

 $\tau^{e}_{CCCH} = \frac{2\tau^{i}_{CCCH}}{1 + n_{i}^{2} / p^{2}}$ 

*n*-region: 
$$\tau^{h}_{CCCH} = \frac{2\tau^{i}_{CCCH}}{1+n^{2}/n_{i}^{2}}$$
 (3)

$$\tau^{h}_{CHHL} = \frac{2\tau^{i}_{CHHL}}{1 + n^{2}_{c}/n^{2}} \tag{4}$$

$$\tau^{h}_{CHHS} = \frac{2\tau^{i}_{CHHS}}{1 + n^{2}_{i}/n^{2}} \tag{5}$$

*p*-region:

$$\tau_{CHHL}^{e} = \frac{2\tau_{CHHL}^{i}}{1 + p^{2}/n_{i}^{2}}$$
(7)

 $\tau_{CHHS}^{e} = \frac{2\tau_{CHHL}^{i}}{1 + p^{2}/n_{i}^{2}}$ (8)

 $n_i$  and  $\tau^i$  indicate intrinsic carrier concentration and recombination time.

The radiative lifetime of minority carriers is given by:

(*n*-region) 
$$\tau^{h}_{Rad} = \frac{1}{B(n + n_i^2 / n)}$$
(9)

(*p*-region) 
$$au_{Rad}^{e} = \frac{1}{B(p + n_i^2 / p)}$$
 (10)

*B* is defined as:

$$B = 5.8 \times 10^{-13} \varepsilon_{\infty}^{1/2} \left(\frac{1}{m_e^* + m_h^*}\right)^{3/2} \left(1 + \frac{1}{m_e^*} + \frac{1}{m_h^*}\right) (300/T)^{3/2} Eg^2$$
(11)

Therefore, diffusion current for both Auger recombination mechanism and radiative mechanism can be obtained as [11]:

$$J_{Diff}^{h} = \frac{qn_{i}^{2}}{N_{D}} \frac{D_{h}}{L_{h}} \frac{\gamma_{h}ch\frac{(t-W_{n})}{L_{h}} + sh\frac{(t-W_{n})}{L_{h}}}{\gamma_{h}sh\frac{(t-W_{n})}{L_{h}} + ch\frac{(t-W_{n})}{L_{h}}} (e^{\frac{qV}{kT}} - 1)$$
(n-region) (12)

(n-region)

(6)

$$J_{Diff}^{e} = \frac{qn_{i}^{2}}{N_{A}} \frac{D_{e}}{L_{e}} \frac{\gamma_{e}ch\frac{(d-W_{p})}{Le} + sh\frac{(d-W_{p})}{L_{e}}}{\gamma_{e}sh\frac{(d-W_{p})}{L_{e}} + ch\frac{(d-W_{p})}{L_{e}}} (e^{\frac{qV}{kT}} - 1)$$
(p-region) (13)

where  $D_i = kT \mu_i / q$ ,  $Li = (D_i \tau_i)^{1/2}$  and  $\gamma_i = L_i S_i / D_i$ , the angle mark *i* namely represents *e* or *h*. *L*, *S*,  $\mu$ , *D* and  $\tau$  are the diffusion length (cm), surface recombination velocity  $(ms^{-1})$ , effective mobility  $(cm^2V^1s^{-1})$ , diffusion coefficient  $(cm^2 s^{-1})$ , and carrier lifetime (s) for holes in the *n* region or for electrons in the p region, respectively.  $n_i$  is the intrinsic carrier concentration ( $cm^{-3}$ ).  $N_D$  and  $N_A$  are donor and acceptor concentrations in p and n regions, respectively.

Due to  $R_0 A$  product can be expressed as

$$\frac{1}{R} = \frac{dI}{dV}\Big|_{V=0} = A \; \frac{dJ}{dV}\Big|_{V=0}$$
(14)

A is device sectional area. The  $R_0A$  product in the *n* and p regions is given respectively by

$$(R_{0}A)_{Diff}^{h} = \frac{kT}{q^{2}} \frac{L_{h}n}{D_{h}n_{i}^{2}} \frac{\gamma_{h}sh(\frac{t-W_{n}}{L_{h}}) + ch(\frac{t-W_{n}}{L_{h}})}{\gamma_{h}ch(\frac{t-W_{n}}{L_{h}}) + sh(\frac{t-W_{n}}{L_{h}})}$$
(n-region) (15)

(*n*-region)

$$(R_{0}A)_{Diff}^{e} = \frac{kT}{q^{2}} \frac{L_{e}p}{D_{e}n_{i}^{2}} \frac{\gamma_{e}sh(\frac{d-W_{p}}{L_{e}}) + ch(\frac{d-W_{p}}{L_{e}})}{\gamma_{e}ch(\frac{d-W_{p}}{L_{e}}) + sh(\frac{d-W_{p}}{L_{e}})}$$
(p-region) (16)

The diffusion current contributions from the n and pregions are added to give the total diffusion current, and the total  $R_0 A$  product from both sides is

$$\frac{1}{(R_0 A)_{D\,iff}^{T\,o\,t\,a\,\overline{l}}} = \frac{1}{(R_0 A)_{D\,iff}^e} + \frac{1}{(R_0 A)_{D\,iff}^h}$$
(17)

#### 2.2 Generation-recombination mechanism

In depletion region, defects and impurities are regarded as intermediate states for the thermal generation and recombination of carriers. These G-R centers are referred as Shockley Read Hall (SRH) centers. The current

caused by generation-recombination mechanism can be approximated as [9]:

$$J_{GR} = \frac{2KTn_iWsh(qV/2kT)}{\tau_{SRH}(V_{bi} - V)}$$
(18)

W is the depletion region width which is dependent on the voltage.  $V_{bi}$  is built-in potential,  $\tau_{SRH} = 1/v_{th}\sigma N_f$  is generation-recombination lifetime of SRH. v<sub>th</sub> is the thermal carrier velocity,  $\sigma$  is the capture cross-section,  $N_f$  is the SRH trap density.

The associated  $(R_0A)_{GR}$  derivatives as:

$$(R_0 A)_{GR} = \frac{V_{bi}}{q n_i W v_{th} \sigma N_f}$$
(19)

#### 2.3 Tunneling mechanism

There are two kinds of tunneling current cross the p-njunction, namely, indirect and direct tunneling current. Because the probability for direct tunneling is much larger than that of indirect tunneling, thus only direct tunneling has been considered in this paper. The tunneling current is given by [12, 13]:

$$J_{Tunnel} = \frac{qm^*}{8\pi^2\hbar^3} T_t \frac{qV}{kT} (\delta_n + \delta_p - qV)^2 \quad (20)$$

 $\delta_n$  and  $\delta_p$  are the distance between Fermi levels and each side of the junction;  $T_t$  is tunneling probability, which is determined by potential barrier shape. For triangular and parabolic barriers, tunneling probability can be expressed as:

$$T_{t1} = \exp(-\frac{4\sqrt{2m^* Eg^{3/2}W}}{3q\hbar V_{bi}})$$
  
lar barriers) (21)

(Triangular barriers)

$$T_{t2} = \exp(-\frac{\pi\sqrt{m^* Eg^{3/2}W}}{2\sqrt{2}q\hbar V_{bi}})$$

(22)

(Parabolic barriers)

Therefore,  $R_0A$  product is derived from above equations.

$$(R_0 A)_{T u n n} = \frac{8\pi^2 \hbar^3 kT}{q^2 m^* T_t (\delta_n + \delta_p)^2}$$
(23)

Material parameters of In<sub>1-x</sub>Ga<sub>x</sub>As ternary-alloy calculated are obtained by method of linear interpolation. The related material parameters are listed in Table 1.

	InAs	GaAs
Eg(T)(eV)	$0.420 - 2.5010^{-4} T^2 / (T + 75)$	$1.519 - 5.4010^{-4} T^2 / (T + 204)$
$\mathcal{E}_r$	14.5	13.18
$m_e^*/m_0$	0.023	0.067
$m_h^*/m_0$	0.41	0.45
$m_s^*/m_0$	0.089	0.15
Δ	0.38	0.34

Table 1. Material parameters used in the calculation [14].

# 3. Results and analysis

Four kinds of noise mechanisms have been effected by material parameters of photovoltaic detectors. We analyzed the influences of carrier concentrations, thickness and surface recombination velocities in the two quasi-neutral regions on  $R_0A$  product. The calculation is performed on a *p*-*n* type of  $In_{0.53}Ga_{0.47}As$  deposited on InPsubstrate.  $D^*$  (Detectivity), a figure of merit of photodetecters, is limited by zero bias resistance-area product ( $R_0A$ ), when assuming quantum efficiency  $\eta = 1$ . In calculation, mobility for the electron and hole are  $\mu_e=5000 cm^2/V \cdot s$  and  $\mu_p=400 cm^2/V \cdot s$ , respectively.

Fig. 2 shows the variations of the theoretically estimated components of R<sub>0</sub>A product (Auger, GR, Rad and Tunnel) and  $(R_0A)_{Total}$  with the doping concentration. Fig. 2 (a) and Fig. 2 (b) correspond to the triangular and parabolic potential barriers, respectively. It exactly shows that tunneling mechanism appears in  $p>10^{18}cm^{-3}$ . This attributes to one necessary requirement for directly tunneling current that both *p*-region and *n*-region must be degenerate.  $(R_0A)_{Tunnel}$  sharply drops with increasing the p-region carrier concentration. Fig. 2 presents that  $(R_0A)_{Total}$  is mainly effected by  $R_0A$  product components in three different ranges, located at low doping concentration range  $(p < 10^{15} cm^{-3})$ , high doping concentration range  $(p>10^{18}cm^{-3})$  and  $10^{15}cm^{-3}< p<10^{18}cm^{-3}$ , respectively. Comparing the Fig. 2 (a) with Fig. 2 (b),  $(R_0A)_{GR}$  mainly contributes to  $(R_0A)_{Total}$  in  $p < 10^{15} cm^{-3}$ , and then tends to saturate at very high doping concentration  $(p>10^{19}cm^{-3})$ . Furthermore, all the  $R_0A$  product components except for the tunneling mechanism have impacted on  $(R_0A)_{Total}$  when  $10^{15} cm^{-3} . This is because that the width of the$ depletion region is comparatively large causing the diffusion and generation-recombination component of current. In this doping range,  $R_0A$  component due to tunneling has a much higher value as compared to the other components (Auger, Rad and GR). However,  $(R_0A)_{Total}$  is limited by the Auger mechanism on the triangular barrier (a) and by the tunneling mechanism on the parabolic barrier (b) in high p-region concentration  $(p>10^{18}cm^{-3})$ . For parabolic barrier, the tunneling component of  $R_0A$  falls below the GR component. At even higher doping concentration, the tunneling component of the  $R_0A$  product also falls below the Auger and Rad component. At higher doping levels of the active region, the width of the depletion region decreases significantly and the tunneling component of current starts to dominate over other components. In order to achieve a high value of  $R_0A$  product, it is therefore necessary to maintain a low doping concentration in the active region.  $(R_0A)_{Total}$ reaches about  $10^6(\Omega \cdot cm^2)$  when *p* is about  $10^{17}cm^{-3}$ , which is consistent with experimental values reported by Antoni Rogalski et al [15].



Fig. 2.  $(R_0A)_{Total}$  and  $R_0A$  product components:  $(R_0A)_{Augers}$  $(R_0A)_{GR}$   $(R_0A)_{Rad}$  and  $(R_0A)_{Tunnel}$  versus the p-region carrier concentration (a) for triangular potential barriers and (b) for parabolic potential barriers.  $t=5\mu m$ ,  $d=5\mu m$ ,  $S_e=0$ ,  $S_h=0$ .

Fig. 3 compares the ultimate  $R_0A$  product of *p*-on-*n* InGaAs photodetector with attainable experimental data [16] for wavelength from 1.2µm to 2.6µm. InGaAs photodetector shows high device performance close to theoretical limits for material whose composition is nearly matched to that of InP ( $\lambda_c \approx 1.7\mu m$ ). However, their performance decreases rapidly at long wavelengths due to mismatch induced defects with the substrate.



Fig. 3. The dependence of  $(R_0A)_{Total}$  product on the wavelength cutoff for p-on-n InGaAs photodetectors at 300K. The experimental values are taken from Ref 16.

The effect of *p*-region carrier concentration on  $R_0A$ product with different *p*-side surface recombination velocity  $(S_e)$  and thickness (d) is shown in Fig. 4. It can be seen from Fig. 4 (a) that  $R_0A$  product decreases with increasing  $S_e$  at range of  $10^{15} cm^{-3} , while the$  $R_0A$  product remains almost constant up to a doping concentration of  $10^{19} cm^{-3}$ . In addition,  $R_0 A$  product has been found to increase with *p*-region carrier concentration, then appear a peak for  $S_e < 10^8$  (m/s). The largest  $R_0A$ product can be obtained about  $R_0A > 10^6 (\Omega \cdot cm^2)$  at  $p=10^{17}cm^{-3}$  when the surface recombination velocity for electrons is assumed to be zero and the peak value is about  $R_0 A > 10^5 (\Omega \cdot cm^2)$  for  $S_e = 100$  (m/s) and  $S_e = 10^4$  (m/s). Reducing surface recombination velocity is benefit to increasing  $R_0A$  product. Therefore, to improve the performance of the detector, surface passivation processes are essential during device fabrication. Fig. 4 (b) depicts the variations of  $R_0A$  product with the p-region concentration as functions of p-region thickness. It distinctly expresses that *p*-region thickness has no effect on  $R_0A$  product at low range carrier concentration  $(p < 10^{15} cm^{-3})$ , and  $R_0 A$  product has been decreased with increasing d when  $10^{15} cm^{-3} . Furthermore, the$  $R_0A$  product of the device increases steadily with increase in doping concentration and reaches a peak value for different d and then finally decreases rather fast with a further increase in doping concentration. The largest value of  $R_0A$  product has been received about  $log(R_0A) > 6.5$  for  $d=0.5 \mu m.$ 



Fig. 4. The effect of p-region carrier concentration on  $R_0A$  product with different (a) p-side surface recombination velocity and (b) thickness.  $t = 5\mu m$ ,  $d = 5\mu m$ ,  $S_h = 0$ .

Fig. 5 shows the dependence of  $R_0A$  product on *n*-region material parameters. The relationship between  $R_0A$  product and *n*-region carrier concentrations with different *n*-side surface recombination velocity  $(S_h)$  at T=250K has been expressed in Fig. 5 (a), and  $R_0A$  product versus the *n*-region carrier concentrations with diverse thickness (t) at T=300K is showed in Fig. 5 (b). The effect of *n*-region parameters on  $R_0A$  product is smaller than the p-region parameters. Fig. 5 (a) explicitly expresses that  $R_0A$  product drops with increasing  $S_h$ , but decreasing value from  $S_h=0(m/s)$  to  $S_h=10(m/s)$  is larger than one from  $S_h=10(m/s)$  to  $S_h=100(m/s)$ .  $R_0A$  product is nearly constant at large surface recombination velocity  $(S_h \ge 10m/s)$ . Furthermore, increasing *n*-region carrier concentrations makes  $R_0A$  product augment, and  $R_0A$  product can be obtained above  $10^8(\Omega \cdot cm^2)$  in  $n > 10^{16} cm^{-3}$ . When  $n=10^{18} cm^{-3}$ , no matter what values of  $S_h$  has been taken,

the value of  $R_0A$  product keeps constant. Fig. 5 (b) depicts that the trend for  $R_0A$  product at different thickness of *n*-region is similar. At the range of  $10^{12}cm^{-3} < n < 10^{15}cm^{-3}$ , varied *t* has no influence on  $R_0A$  product. However,  $R_0A$ product appears slightly drop with increasing *t* within  $10^{15}cm^{-3} < n < 10^{18}cm^{-3}$ . Moreover,  $R_0A$  product increases with increasing *n*, and  $R_0A$  product achieves above  $10^6(\Omega \cdot cm^2)$  in  $n > 10^{16}cm^{-3}$ . As already mentioned, the  $R_0A$ product of the device is strongly influenced by the operating temperature. The value of  $R_0A$  product is  $10^8(\Omega \cdot cm^2)$  at T=250K and  $10^6(\Omega \cdot cm^2)$  at T=300K, respectively, which has been confirmed in the literature of A. Rogalski [17].



Fig. 5. The relationship between n-region carrier concentration on  $R_0A$  product with different (a) n-side surface recombination velocity and (b) thickness.  $t=5\mu m$ ,  $d=5\mu m$ ,  $S_e=0$ .

# 4. Conclusion

Four kinds of noise mechanism have diverse impact on  $(R_0A)_{Total}$  at different range of carrier concentration.  $(R_0A)_{GR}$  determines  $(R_0A)_{Total}$  at low carrier concentration  $(p < 10^{15} cm^{-3})$ . However, when  $p > 10^{18} cm^{-3}$  and both *p*-region and *n*-region to be degenerate,  $(R_0A)_{Total}$  is limited by the Auger mechanism on the triangular barrier and by the Tunneling mechanism on the parabolic barrier. Furthermore, the carrier concentration, thickness and surface recombination velocities in the two quasi-neutral regions have significant influences on  $R_0A$  product. The effect of *n*-region parameters on  $R_0A$  product is smaller than the *p*-region parameters. It is apparent that the  $R_0A$ product increases steadily with increase in *p*-region doping concentration, reaches a peak value and then finally decreases with a further increase in doping concentration. However,  $R_0A$  product has been found to increase with *n*-region carrier concentration and tends to be saturated. In addition, the  $R_0A$  product of the device is strongly influenced by the operating temperature. The value of  $R_0A$ product is  $10^8(\Omega \cdot cm^2)$  at T=250K while it is  $10^6(\Omega \cdot cm^2)$  at T=300K. These results will provide a useful guide for designing and fabrication of the  $In_{0.53}Ga_{0.47}As$  photovoltaic detectors.

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